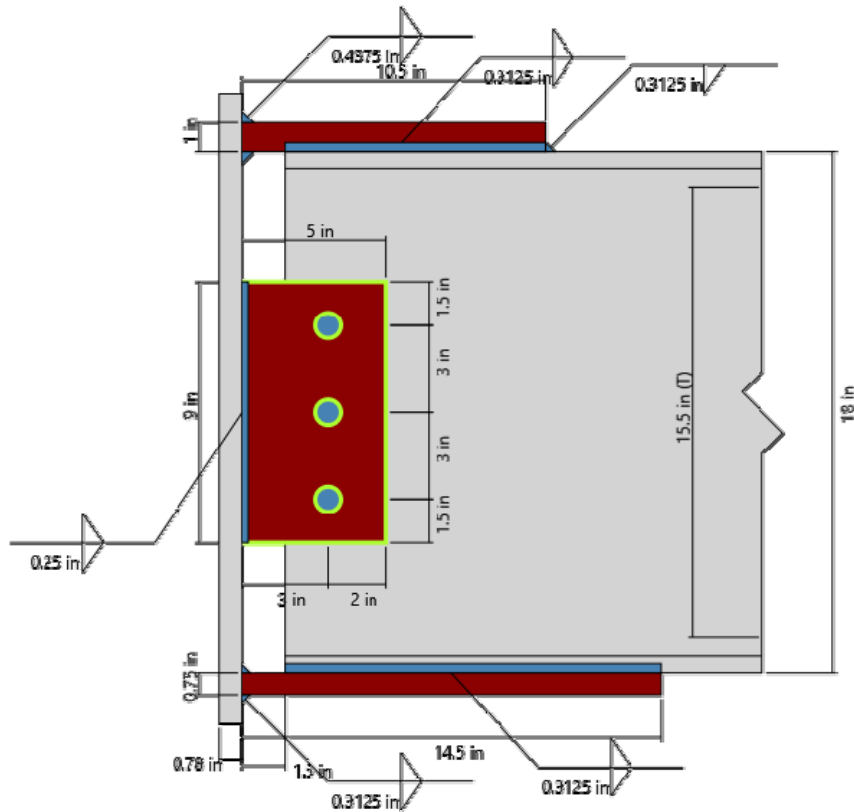


## Design Summary: Welded Flange Plate



### Top Plate Design:

Width = 6 in  
 Fy = 36 Ksi  
 Fu = 58 Ksi

### Support Design:

Thickness = 0.78 in  
 Fy = 50 Ksi  
 Fu = 65 Ksi

### Shear Tab Design:

Thickness = 0.375 in  
 Fy = 36 Ksi  
 Fu = 58 Ksi

### Beam Design:

bf = 7.5 in  
 tf = 0.57 in  
 tw = 0.355 in  
 Fy = 50 Ksi  
 Fu = 65 Ksi

### Bottom Plate Design:

Width = 8.75 in  
 Fy = 36 Ksi  
 Fu = 58 Ksi

### Bolt Design:

Type = Group A  
 Diameter = 0.875 in  
 Thread = N

### Steel Specification:

AISC 360-16

<u>Limit State</u>	<u>Load Key</u>	<u>Demand</u>	<u>Capacity</u>	<u>Unity Value</u>
Bolt Group Shear	1	42 K	73.06 K	0.575
Bolt Group Bearing - Beam Web	1	42 K	136.29 K	0.308
Bolt Group Bearing - Tab	1	42 K	75.7 K	0.555
Fillet Weld - Tab to Support	1	42 K	100.23 K	0.419
Base Metal - Support	1	42 K	410.67 K	0.102
Base Metal - Tab	1	42 K	72.9 K	0.576
Block Shear - Tab	1	42 K	70.031 K	0.600
Shear Yield - Tab	1	42 K	72.9 K	0.576
Shear Rupture - Tab	1	42 K	58.725 K	0.715
Tension Yield - Top Plate	1	166.89 K	194.4 K	0.858
Tension Rupture - Top Plate	1	166.89 K	261 K	0.639
Compression Buckling - Top Plate	0	0 K	194.28 K	0.000
Block Shear - Top Plate to Flange	1	-	-	0.000
Fillet Weld - Top Plate to Flange	1	166.89 K	169.14 K	0.987
Base Metal - Top Flange	1	166.89 K	405.14 K	0.412
Base Metal - Top Plate	1	166.89 K	524.88 K	0.318
Weld - Top Plate to Support	1	166.89 K	175.41 K	0.951
Base Metal - Top Plate to Support	1	166.89 K	194.4 K	0.858
Tension Yield - Bottom Plate	0	0 K	212.63 K	0.000
Tension Rupture - Bottom Plate	0	0 K	249.55 K	0.000
Compression Buckling - Bottom Plate	1	166.89 K	212.4 K	0.786
Block Shear - Bottom Plate to Flange	1	-	-	0.000
Fillet Weld - Bottom Plate to Flange	1	166.89 K	180.98 K	0.922
Base Metal - Bottom Flange	1	166.89 K	433.49 K	0.385
Base Metal - Bottom Plate	1	166.89 K	421.2 K	0.396
Weld - Bottom Plate to Support	1	166.89 K	182.72 K	0.913
Base Metal - Bottom Plate to Support	1	166.89 K	399.26 K	0.418
Welded Flange Plate Detailing	-	-	-	OK

## Welded Flange Plate: Detailed Reports

### Tension Yield - Top Plate(AISC 360-16 J4.1.a)

Load Set: Load Set 1 Load Combination: 1.2D + 1.6L

Demand:  $R_u = 166.89 \text{ K}$

Capacity:  $\phi R_n = \phi \cdot F_y \cdot b \cdot t = 0.90 \cdot 36 \text{ Ksi} \cdot 6 \text{ in} \cdot 1 \text{ in} = 194.4 \text{ K}$

Unity =  $R_u / \phi R_n = 166.89 \text{ K} / 194.4 \text{ K} = \mathbf{0.858}$

**Fillet Weld - Top Plate to Flange (AISC 360-16 J2.4)**

Load Set: Load Set 1 Load Combination: 1.2D + 1.6L

Demand:  $R_u = 166.89 \text{ K}$

Weld: Size = 0.3125 in  $F_{exx} = 70 \text{ Ksi}$

Longitudinal Length = 9 in Transverse Length = 6 in

$R_{n\_wl} = 167.05 \text{ K}$   $R_{n\_wt} = 55.685 \text{ K}$  Weld Unit Capacity = 111.37 K/ft

$\phi R_n = \text{Phi} \cdot \text{Max}(R_{n\_wl} + R_{n\_wt}, 0.85 \cdot R_{nwl} + 1.5 \cdot R_{nwt})$  (Equation J2-6a & J2-6b)

$\phi R_n = \text{Phi} \cdot \text{Max}(167.05 \text{ K} + 55.685 \text{ K}, 0.85 \cdot 167.05 \text{ K} + 1.5 \cdot 55.685 \text{ K})$

$\phi R_n = 169.14 \text{ K}$  (Equation J2-6a & J2-6b)

Unity =  $R_u / \phi R_n = 166.89 \text{ K} / 169.14 \text{ K} = \mathbf{0.987}$

**Weld - Top Plate to Support (AISC 360-16 J2.4)**

Load Set: Load Set 1 Load Combination: 1.2D + 1.6L

Demand:  $R_u = 166.89 \text{ K}$

Fillet Weld: Size = 0.4375 in  $F_{exx} = 70 \text{ Ksi}$  Weld Length = 6 in Theta = 90 deg

Weld Line Count = 2 Weld Unit Capacity = 233.88 K/ft

$\phi R_n = \text{Phi} \cdot 0.6 \cdot F_{exx} \cdot (1.0 + 0.5 \cdot \sin(\text{Theta})^{1.5})$  (Equation J2-4)

$\phi R_n = 0.75 \cdot 0.6 \cdot 70 \text{ Ksi} \cdot (1.0 + 0.5 \cdot \sin(90 \text{ deg})^{1.5})$

$\phi R_n = 175.41 \text{ K}$

Unity =  $R_u / \phi R_n = 166.89 \text{ K} / 175.41 \text{ K} = \mathbf{0.951}$

**Base Metal - Top Plate to Support (AISC Part 9 & 360-16 J2.4)**

Load Set: Load Set 1 Load Combination: 1.2D + 1.6L

Demand:  $R_u = 166.89 \text{ K}$  (Tension)

Weld: Weld Length = 6 in

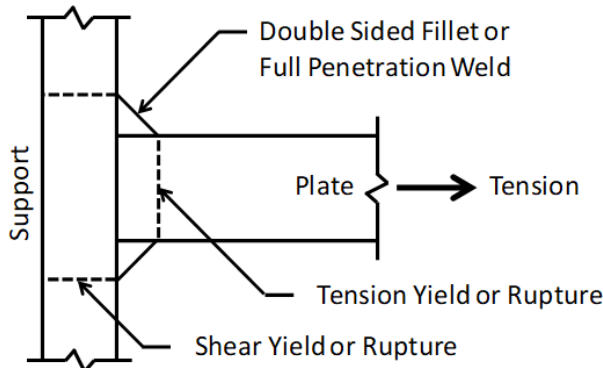


Plate:  $F_y = 36 \text{ Ksi}$   $F_u = 58 \text{ Ksi}$   $t = 1 \text{ in}$

Tensile Yield:  $\phi R_{n\_ty} = 0.9 \cdot F_y \cdot t \cdot \text{WeldLength} = 194.4 \text{ K}$  (Equation J4-1)

Tensile Rupture:  $\phi R_{n\_tr} = 0.75 \cdot F_u \cdot t \cdot \text{WeldLength} = 261 \text{ K}$  (Equation J4-2)

Capacity:  $\phi R_{n1} = \text{Min}(\phi R_{n\_ty}, \phi R_{n\_tr}) = 194.4 \text{ K}$

Support:  $F_y = 50 \text{ Ksi}$   $F_u = 65 \text{ Ksi}$   $t = 0.78 \text{ in}$

Shear Yield:  $\phi R_{n\_vy} = 1.0 \cdot 0.6 \cdot F_y \cdot t \cdot \text{WeldLength} \cdot 2 = 280.8 \text{ K}$  (Equation J4-3)

Shear Rupture:  $\phi R_{n\_vr} = 0.75 \cdot 0.6 \cdot F_u \cdot t \cdot \text{WeldLength} \cdot 2 = 273.78 \text{ K}$  (Equation J4-4)

Capacity:  $\phi R_{n2} = \text{Min}(\phi R_{n\_vy}, \phi R_{n\_vr}) = 273.78 \text{ K}$

Unity =  $R_u / \text{Min}(\phi R_{n1}, \phi R_{n2}) = 166.89 \text{ K} / 194.4 \text{ K} = \mathbf{0.858}$

### **Compression Buckling - Bottom Plate (AISC 360-16 E3)**

Load Set: Load Set 1 Load Combination: 1.2D + 1.6L

Demand: Ru = 166.89 K

Plate: Fy = 36 Ksi Thickness = 0.75 in Ag = 6.5625 in<sup>2</sup> K = 0.65 L = 1.5 in r = 0.21651 in

Capacity:

KL/r = 4.503 Fe = 14113 Ksi (Equation E3-4) Fcr = 35.962 Ksi (Equation E3-2)

φRn = φ · Ag · Fcr = 0.90 · 6.5625 in<sup>2</sup> · 35.962 Ksi = 212.4 K

Unity = 166.89 K / 212.4 K = **0.786**

### **Fillet Weld - Bottom Plate to Flange (AISC 360-16 J2.4)**

Load Set: Load Set 1 Load Combination: 1.2D + 1.6L

Demand: Ru = 166.89 K

Weld: Size = 0.3125 in Fexx = 70 Ksi

Longitudinal Length = 13 in Transverse Length = 0 in

Rn\_wl = 241.3 K Rn\_wt = 0 K Weld Unit Capacity = 111.37 K/ft

φRn = Phi · Max(Rn\_wl + Rn\_wt, 0.85·Rnwl + 1.5·Rnwt) (Equation J2-6a & J2-6b)

φRn = Phi · Max(241.3 K + 0 K, 0.85·241.3 K + 1.5·0 K)

φRn = 180.98 K (Equation J2-6a & J2-6b)

Unity = Ru / φRn = 166.89 K / 180.98 K = **0.922**

## **Load Combinations**

Code	Name	Effective Equation
ASCE 7-16 LRFD	1. 1.4D	1.4D
ASCE 7-16 LRFD	2. 1.2D+1.6L+0.5Lr	1.2D + 1.6L
ASCE 7-16 LRFD	3. 1.2D+1.6Lr+L	1.2D + 0.5L

## **Design Loads**

Load Key	Fvu (K)	Fau (K)	Mzu (K-ft)
0	-9.8	0	-58.8
1	-42	0	-252
2	-18.9	0	-113.4